3D FEA COMPUTATION OF THE CLIC MACHINE DETECTOR INTERFACE MAGNETS

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Abstract

A critical aspect of the Compact Linear Collider (CLIC) design is represented by the Accelerator/Experiment interface (called Machine Detector Interface or MDI). In the 3 TeV CLIC layout, the final focus QD0 quadrupole will be located inside the end-cap of the detector itself. This complex MDI scenario required to be simulated with a full 3D-FE analysis. This study was critical to check and control the magnetic cross-talk between the detector solenoid and the final focus magnet and therefore to optimize the design of an "antisolenoids" system needed to shield the QD0 and the e^-/e^+ beams from the detector magnetic field. In this paper the development and evolution of the computational FE model is presented together with the results obtained and their implication on the CLIC MDI design.

INTRODUCTION

One of the challenges related to the design of the compact Silicon Detector CLIC SiD, comes from the parameter L^*, which represents the distance between the Interaction Point (IP) and the last magnet of the Beam Delivery System. With a baseline L^* value of 3.5 m, the final focus magnet QD0 must be placed *inside* the detector, precisely within the limits of the yoke end-cap.

Since QD0 is an *ferromagnetic* quadrupole which also contains permanent magnets, an active shielding (provided by an "anti-solenoid") is necessary to limit the interaction with the detector main solenoid field, as this could lead to a degradation of the quadrupole performance in terms of gradient and to an increase of the magnetic forces on QD0.

In the final stage of the CLIC Conceptual Design Report preparation, after having already simulated the detector with 2D models and having defined an integrated layout of the various detector components, a 3D model of the MDI region (represented in figure 1) was proposed, to correctly simulate all the magnets and ferromagnetic parts influencing this region. The aim of this model is to help in the correct dimensioning and integration of the anti-solenoid system, by investigating its magnetic relations with the main solenoid, the detector and the QD0, as well as its impact on the beam dynamic and on the supporting structure, in terms of both magnetic field and forces.

THE 3D MODEL

The 3D model was adopted after extensive studies with 2D models representing the detector with both the main solenoid and the anti-solenoid [1]. In fact, while it is possible to use an axial symmetric model to approximate the iron yoke and the detector and anti-solenoid coils, such a
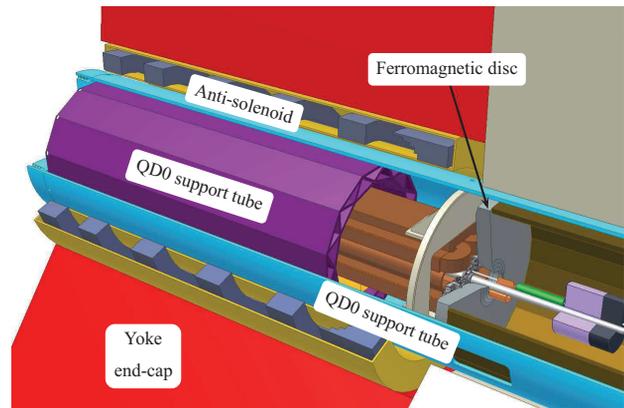
Figure 1: The CLIC SiD MDI Region.

simplification is not at all compatible with QD0, which requires a 3D model to be simulated. On the other hand, even if the introduction of the full magnet in the model will make the computation heavier, this allows to evaluate directly the performance (gradient) that QD0 can develop in the realistic MDI conditions.

Model Description

The software chosen for the simulation is Opera3D™. Due to the nature of the problem, there is just one plane of symmetry that can be used: the one passing by the IP, perpendicular to the detector axis. So the model to be simulated is made of a half of the detector yoke, plus one of the two QD0 held in the experiment. The most challenging aspect of such model is the scale difference: in the same simulation coexist in fact objects as big as the iron yoke (shown in figure 2), which has a "radius" of 7 m and a half-
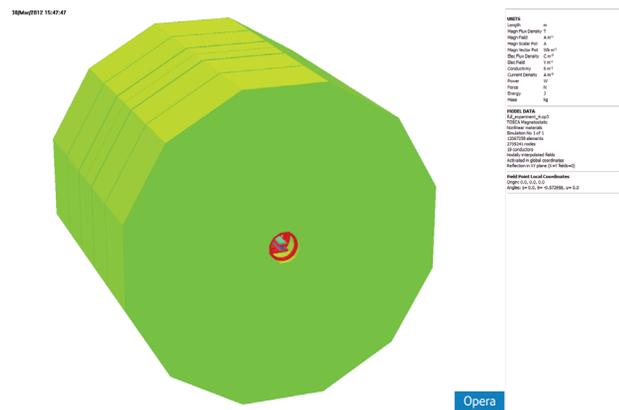
Figure 2: The CLIC SiD 3D model.

length of 6.2 m, and QD0 (shown in figure 3), which has an aperture radius of just 4.125 mm. Moreover, the field in the QD0 aperture is the most relevant quantity, but due to meshing convergence problems, and to computation time, the precision of the results is lower than the one achievable by models representing the single magnet only.

Finally, due to the *hybrid* design of QD0 [2], permanent magnets, soft ferromagnetic region, normal conducting racetrack coils and super-conducting solenoids have to be included all at once in the same simulation.
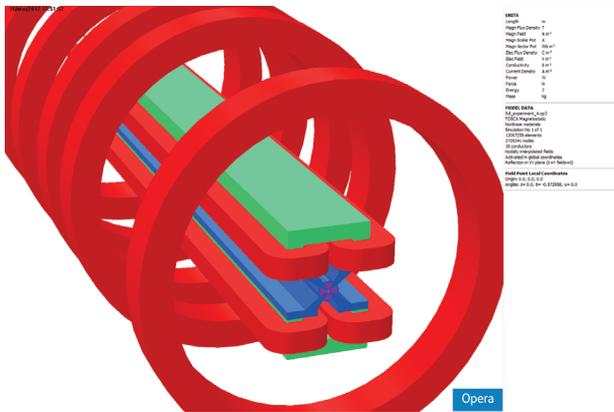
Figure 3: A detail of QD0 inside the anti-solenoid.

Results

In terms of field on the beam axis, the resulting component B_z is plotted in figure 4, and B_r is shown in figure 5. The effect of QD0 on the beam axis is beneficial, since its ferromagnetic structure *shields* the beam from the surrounding fields. Such results are visibly affected by a numeric error due to the element size, so they were averaged before being used for beam dynamics simulations. This averaging may appear unjustified, but it was necessary, considering the nature of the problem and the FE model features. The luminosity loss due to the new field maps is
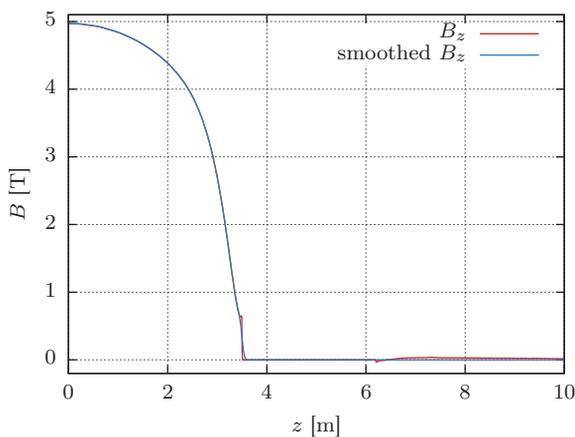
$\simeq$14%, which is compatible with any other previous CLIC SiD design simulated so far [3].

Finally, such model permitted to evaluate the forces acting on the anti-solenoid, which are not affected by the introduction of QD0, and remained equal to the ones evaluated in the 2D case: the most relevant is the axial force F_z of $7.0 \cdot 10^6$ N acting on the first coil of the anti-solenoid, pushing it away from the IP.

THE QD0 IN DETAIL

As already anticipated, one of the most noticeable advantage of the whole 3D simulation is the possibility to study in detail the interactions between QD0 and the detector magnetic field. This permitted to improve the anti-solenoid design established with 2D simulations, by adjusting its current in order to balance the higher field attracted by the QD0 in the yoke end-cap region.

This adjustment consisted in an iterative process in which new coil dimensions and currents of the anti-solenoid were proposed, simulated and then evaluated by comparing the performance of QD0 in the different cases. During such procedure it was noticed that without making any change in the overall layout, the innermost area of QD0 could be unable to develop the required gradient. Figure 6 shows the axial field attracted by the QD0 in case of an anti-solenoid layout compatible with the CLIC baseline. Such results (up to 3 T of external field entering the QD0 poles) are not compatible with the correct functioning of the magnet, so a solution is being proposed.

A Proposed Solution

A better QD0 performance was achieved by moving the anti-solenoid towards the IP and adjusting its coil shapes and currents [1]. Figure 7 shows the field attracted by QD0 in this solution, while the gradient it developed across its length is plotted in figure 8. Such gradient is measured along four lines parallel to the beam axis, placed at a distance of 1 mm from it either in the $\pm x$ or the $\pm y$ directions. A slight decrease of the gradient in the innermost region of

Figure 4: Axial component of the field on the beam axis.
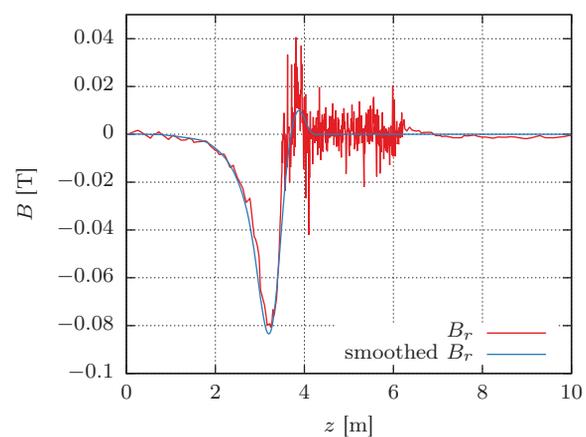
Figure 5: Radial component of the field on the beam axis.
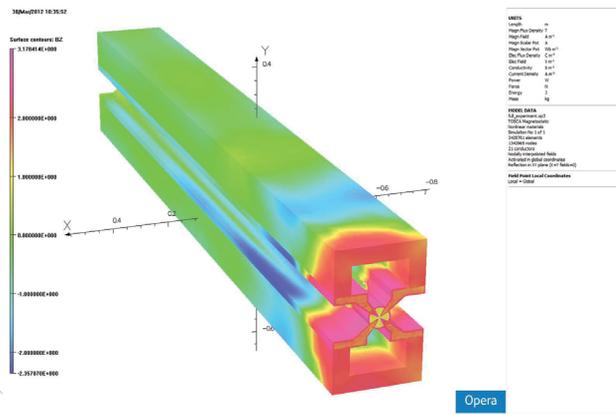
Figure 6: The axial field in the QD0 structure.
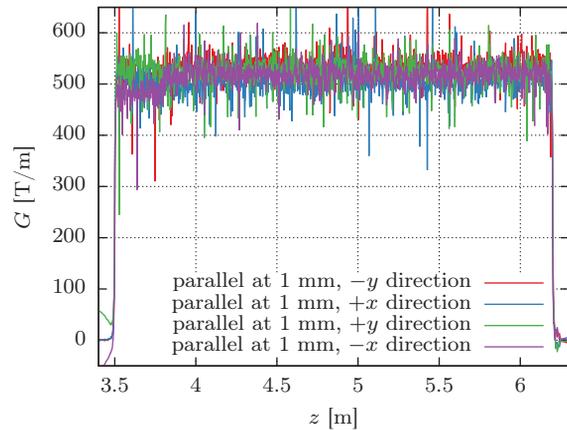
Figure 8: QD0 gradient on four parallels to the beam axis.

the magnet is still visible, but the integrated gradient differed by less thatn 5% from the requirements, which is acceptable given the R&D status of the detector study.

This case was also studied by the mechanical point of view, and the magnetic forces acting on QD0 are estimated as $F_z \simeq -5.7$ kN, $F_x \simeq 8.3$ kN and $T_y \simeq 5.6 \cdot 10^3$ Nm.

Finally, to demonstrate the efficiency of the anti-solenoid solution, a last configuration was investigated, not intended to be compliant with the CLIC beam delivery system baseline, as it is based on an L^* increased by 0.3 m (from 3.5 m to 3.8 m). The QD0 gradient obtained is plotted in figure 9, and its integral differs by less than 1% to the specifications, which is less than the accuracy of the model itself.

tems on the incoming beam, it can be noticed that the luminosity loss is *coherent* with all the previous designs and it is related mainly to the radial component of the field in the region between QD0 and the IP.

ACKNOWLEDGMENT

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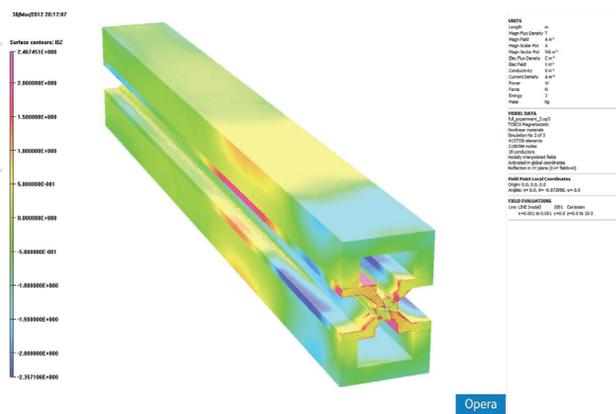
Figure 7: The axial field in the QD0 structure, with the newly proposed anti-solenoid.
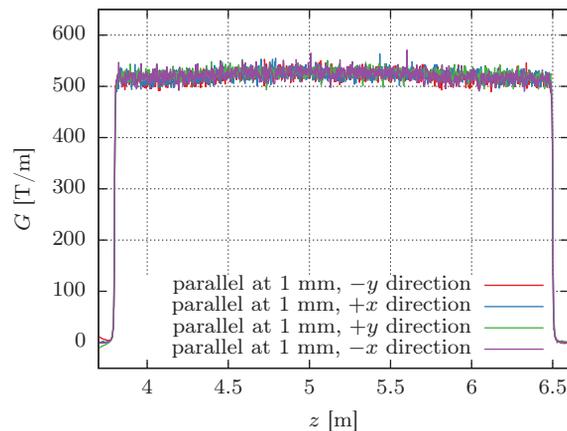
Figure 9: QD0 gradient on axis parallels, with $L^* = 3.8$ m.

CONCLUSIONS

The most important achievement of this study was that with an appropriate shielding (i.e. the anti-solenoid) the QD0 *can* work as specifications, even if placed very close to the strong detector magnetic field. On the other hand, to obtain such performances it is necessary an adequate space allocation. A proper shielding of the QD0 also reduces the forces acting on this hybrid electromagnet, making its stabilization easier. Finally, regarding the impact of such sys-

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