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Charge Measurements in SwissFEL and Results of an Absolute Charge Measurement Method

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- Overview of the SwissFEL charge monitors
 - Faraday Cup
 - Integrating Current Transformer
 - Wall Current Monitor
 - Cavity Beam Position Monitor

- Wall Current Monitor: experimental characterization and numerical modelling results

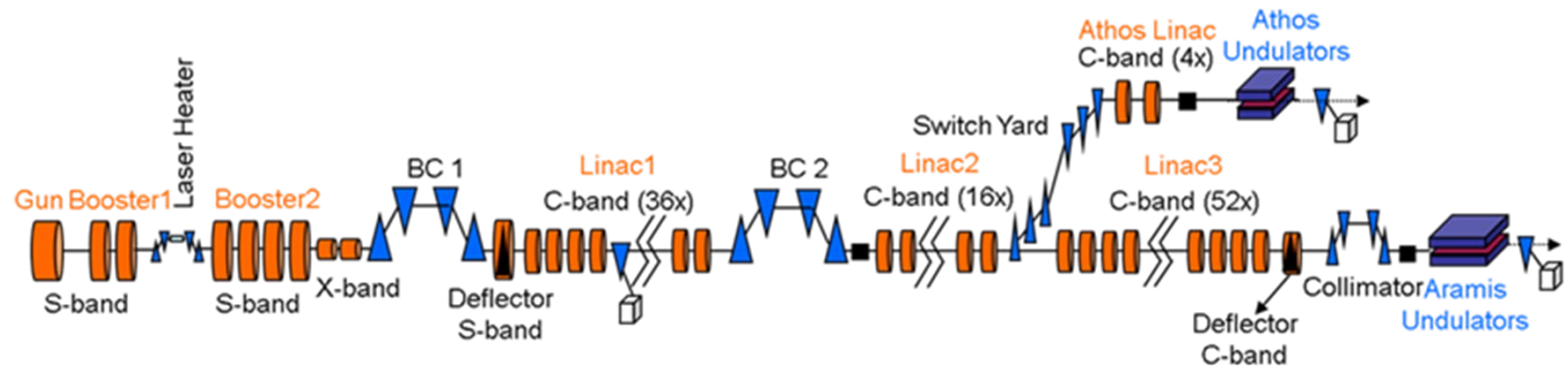
- Cavity Beam Position Monitor for absolute charge measurements

- Charge measurement campaign at SwissFEL

- Procedure for absolute calibration of the SwissFEL charge monitors

- Conclusions

SwissFEL in a sketch



- Beam energy: 6.2 GeV and 3.3 GeV
- Beam charge: 10-200 pC @100Hz, 28 ns 2-bunch time structure
- Emittance: 0.4/0.2 mm mrad
- Bunch length: from a 3 ps up to a few fs
- Photon wavelength: 0.1-0.7 nm and 0.7-7.0 nm

Charge Monitor in SwissFEL

- Turbo ICT (Integrating-Current-Transformer):
 - 4 in Aramis and 2 in Athos
 - 28 ns 2-bunch resolution

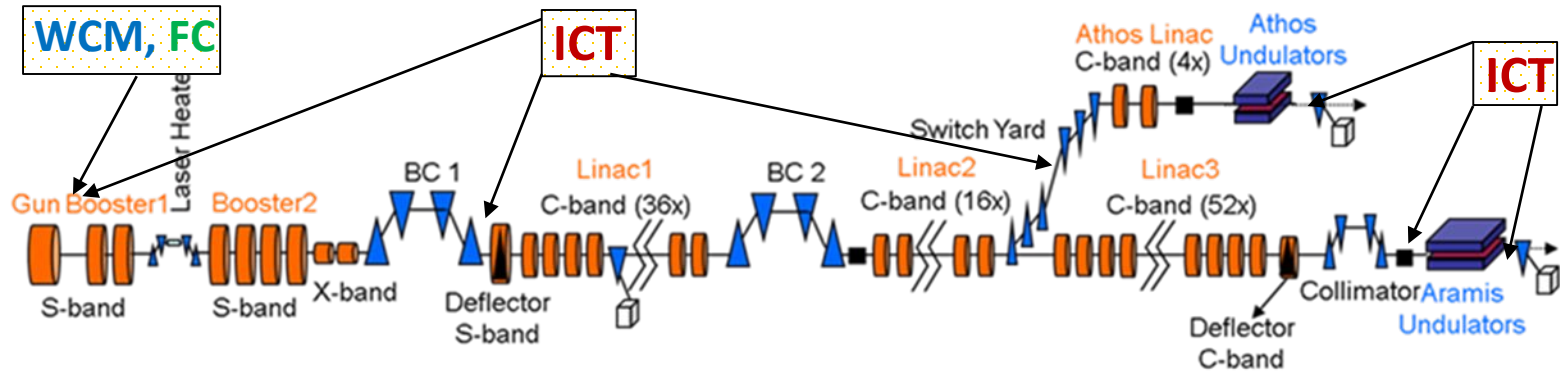
- Standard ICT (1 in the gun section):
 - full beam current integral (no 2-bunch discrimination)

- Cavity-BPM (Beam-Position-Monitor):
 - ~200 units distributed all along Aramis and Athos

- Wall-Current-Monitor (WCM, 1 in the gun section):
 - coarse synchronization photocathode laser timing and RF gun phase
 - 2-bunch charge monitoring @100 Hz

- Faraday- Cup (one unit in the Gun section):
 - Dark current

Integrating Current Transformer (ICT)



➤ Standard ICT (BCM-IHR readout electronics)

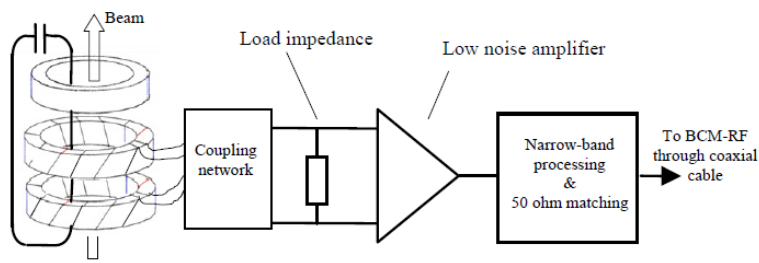
- time integration ($5\mu\text{s}$) of the beam induced current in the transformer
- Broad-band frequency response ($\text{kHz} \rightarrow 10\text{ MHz}$)
- no 2-bunch time structure resolution
- Sensitive to dark current of the gun
- Charge resolution $\sim \text{pC}$



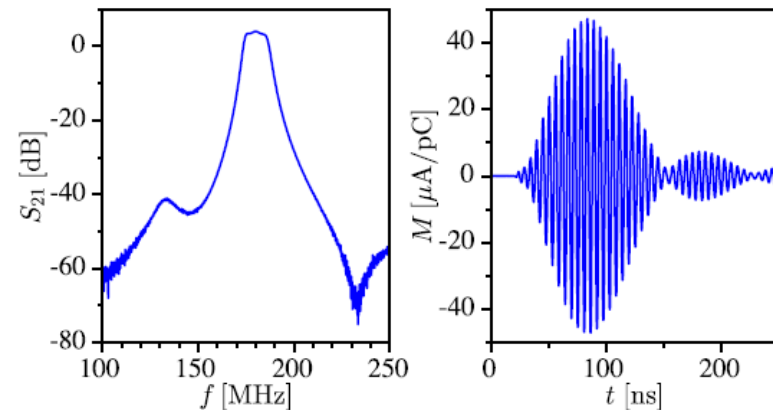
Courtesy Bergoz

➤ **Turbo-ICT2** (BCM-RF readout electronics)

- High frequency transformer (bandwidth up to several hundred MHz)
- Narrow band-pass filter centered at around 180 MHz (resonance quality factor reduced to discriminate the 2 bunch)
- Output signal is a resonance with amplitude proportional to the bunch charge
- Beam charge determined by measuring the apex of the resonance (sample-and-hold electronics)
- 28 ns 2-bunch time structure discrimination and immunity to dark current
- rms resolution 0.1 pC (1%) in the 10-200 pC SwissFEL charge range



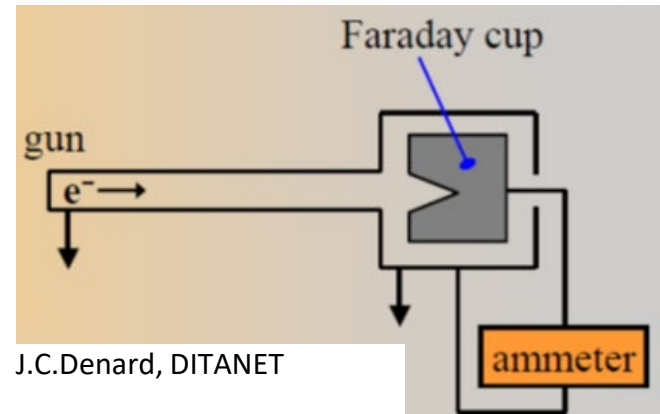
Courtesy Bergoz, Artinian et al IBIC2012



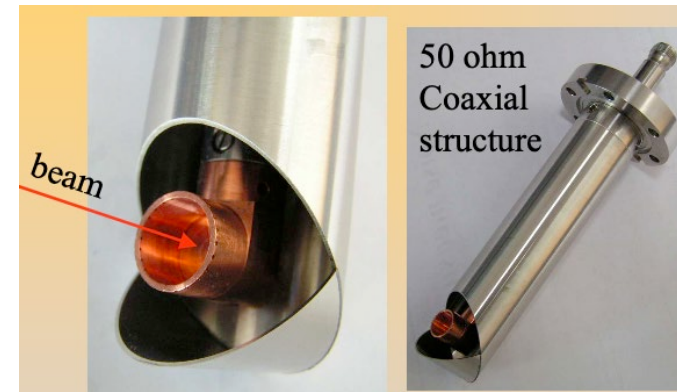
F. Stulle, J. Bergoz, Proc. FEL2015

Faraday Cup (FC)

- The Faraday cup destructively intercepts the beam
- Low current and dark current measurements
- Systematic error in charge measurements:
 - “Containment”: mismatch between e.m. shower and absorber dimensions
 - “Charge trapping”: absence of voltage or magnetic “cage” to bring back secondary and scattered electron
- resistor signal coupled with DC component of input current

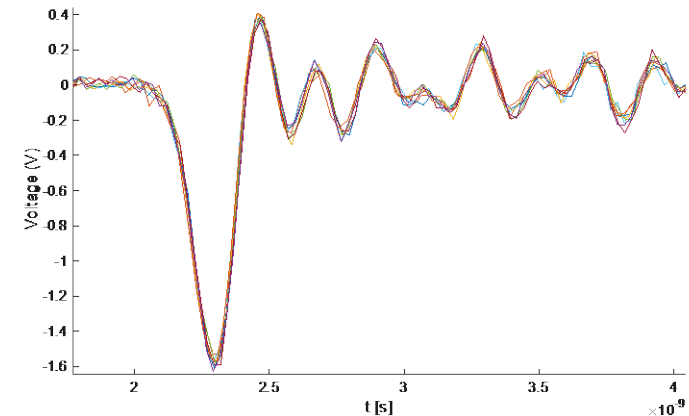
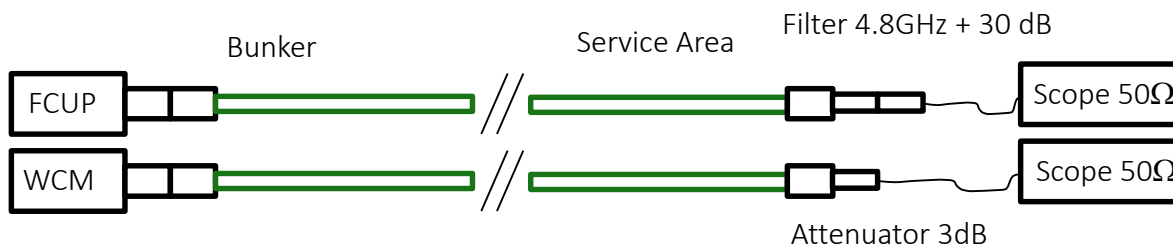


J.C.Denard, DITANET

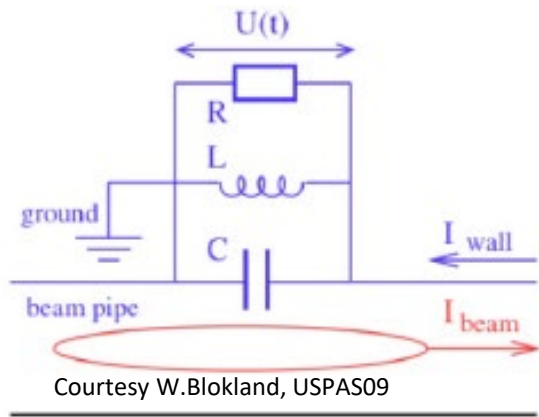


M. Dach et al. (SLS Linac) ; BIW2000

$$Q = \int \frac{v_{fcup}(t)}{R} dt$$



Wall Current Monitor in SwissFEL



Prototype Wall Current Monitor

In WLHA

$R_{gap} = 3.0 \pm 0.05 \Omega$ (2.83Ω with 50Ω)
(12 x 36 Ohm gap resistors)

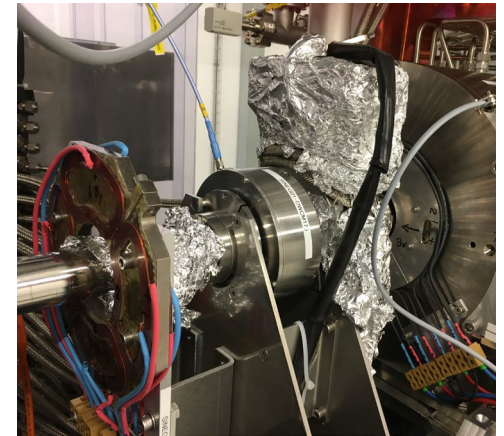
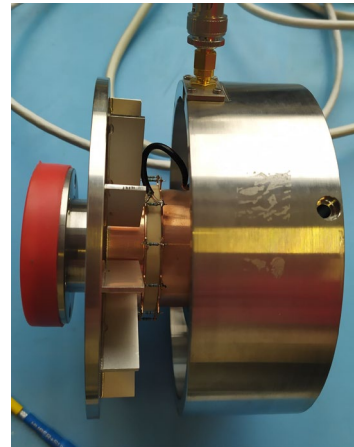
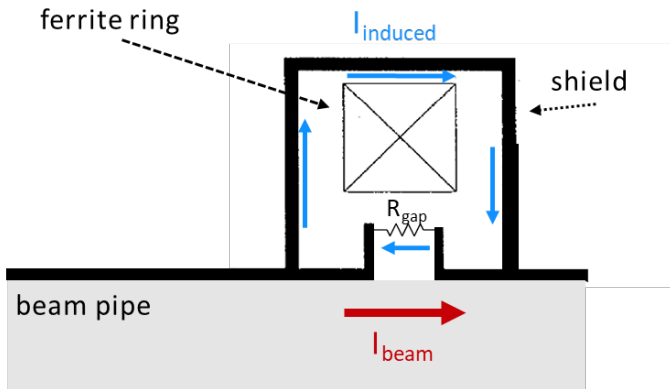
NiZn ferrite ring

SwissFEL Wall Current Monitor

After RF gun (z=0.58 m)

$R_{gap} = ?$

NiZn ferrite ring



$$Q = \frac{1}{R_{gap}} \int V_{R_{gap}}(t) dt$$

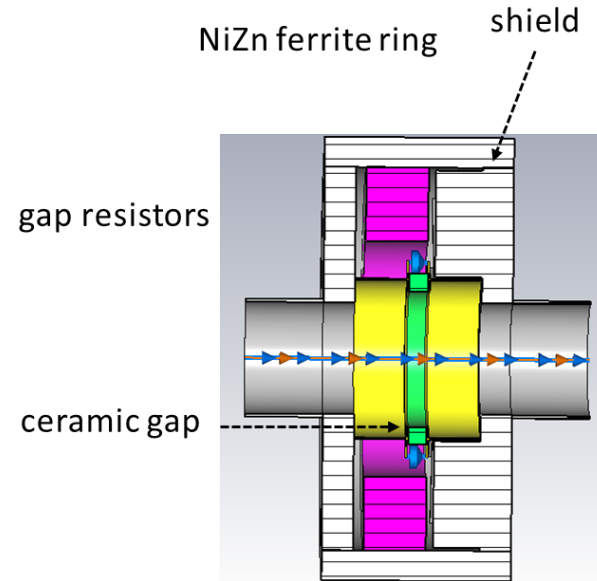
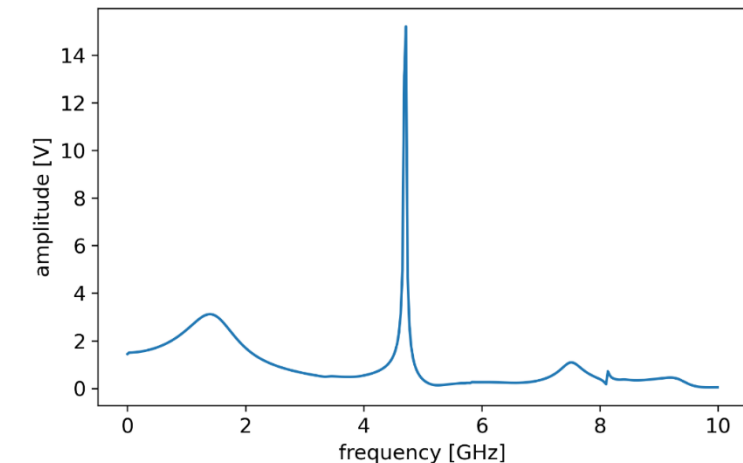
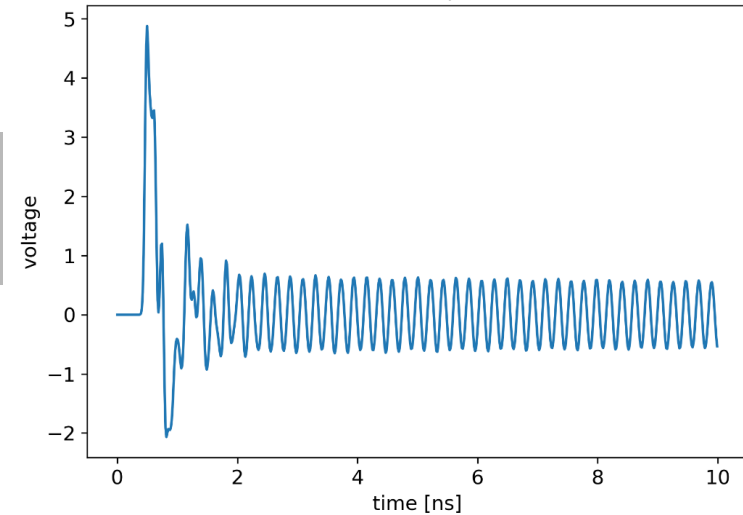
Time integration window ~ 10 ns

Lower cutoff frequency $f_{low} = R_{gap} / 2\pi L \sim 200\text{kHz}$ (no DC component of input current measurable)

Upper cutoff frequency $f_{high} = 1 / (2\pi R_{gap} C) \sim \text{GHz}$

good WCM → flat transfer impedance $Z(\omega) \sim R_{gap}$ in the frequency range of interest (up to hundreds of MHz)

CST Simulation WCM output (25 ps , 200 pC)



time response

- The Gaussian beam signal is distorted due to the upper cutoff frequency
- Voltage oscillations in the resistor (long time regime)

frequency response

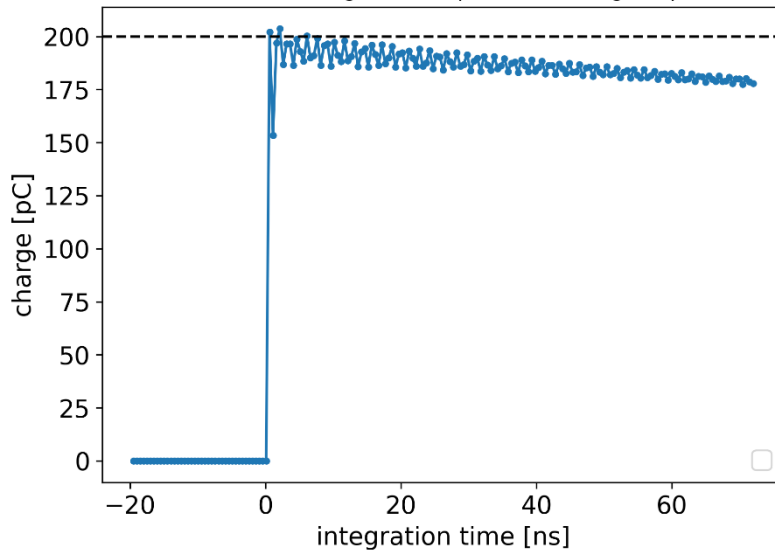
- Approx. constant for $f \ll 1$ GHz
- Broad peak at 1.5 GHz
- Sharp peak at 4.7 GHz (voltage oscillations)

1.5 Gz peak → mismatch of the gap resistance and transmission line capacitive gap

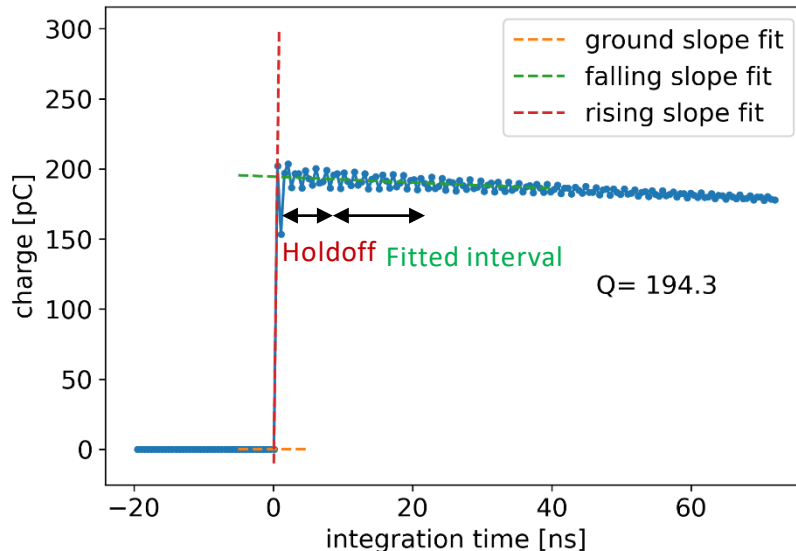
4.7 GHz sharp peak → step transition (radius) from the beam pipe to the gap

Charge Measurement in the simulation

Q = 200 pC, $\tau=25$ ps , 0.5 ns integration steps



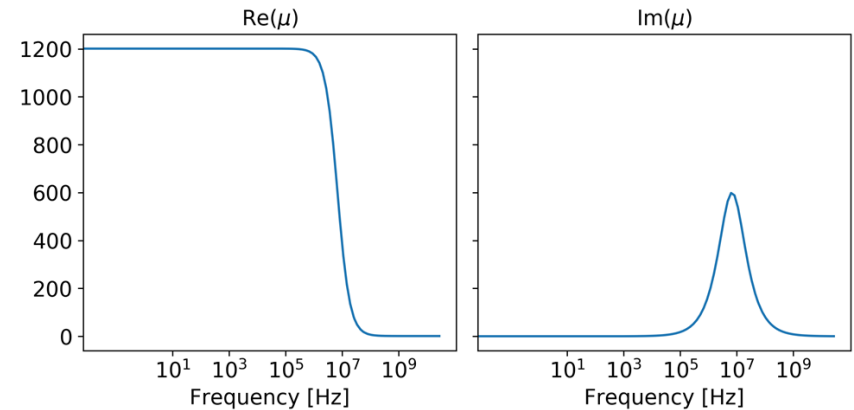
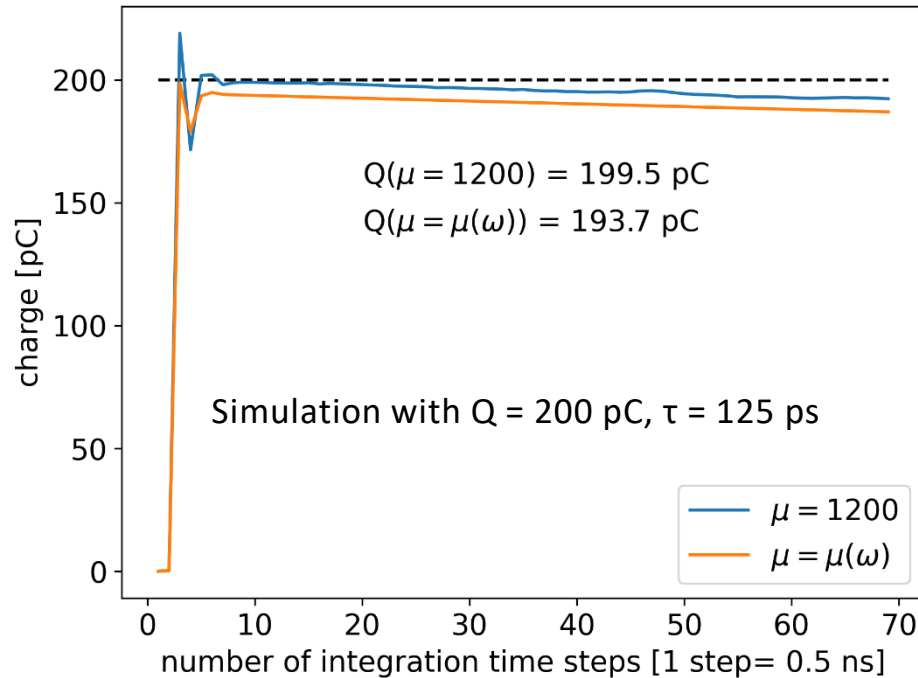
- The measured charge decreases.
 - No DC measurable. For infinite integration time, $Q=0$.
- The slope is determined by the lower cutoff frequency $f_{low} = \frac{R_{gap}}{2\pi L}$
- First few data points after bunch incidence include current components outside the WCM bandwidth (non measurable)



Idea: Make linear fit of slope and intersect fit with the step to reconstruct the charge at the time when the bunch arrives.

- Holdoff (2.5 ns) to avoid first few data points
- Fitted interval = 10 ns

Charge Measurement: the Ferrite Ring



Complex Inductance

$$L(\omega) = L'(\omega) - iL''(\omega).$$

The shield impedance now has a real part

$$Z_L = i\omega L = i\omega L'(\omega) + \omega L''(\omega)$$

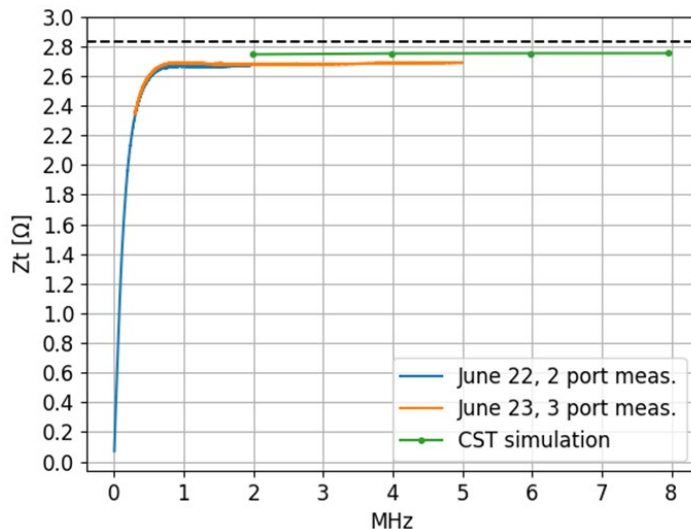
→ Additional frequency dependent ohmic resistor $\omega L''(\omega)$ in series with the shield inductance.

- **Dispersive ferrite yields charge losses, because we only measure the voltage over the gap**
- **Which value of the gap resistance to be used for WCM charge measurement ?**

SwissFEL WCM: gap resistance value?

- Spare WCM prototype → Multimeter inspection and VNA measurements of the reflection coefficient S_{11} at the output port confirmed a gap resistance $R_{gap}=3.0 \Omega$.
- SwissFEL WCM → No inspection possible, VNA measurements of S_{11} → $R_{gap}=3.55 \Omega$.
- Transfer impedance measurements of spare WCM in a test-bench (coaxial wire method):
 - Transfer impedance $Z_t(\omega)$ constant up to several MHz → $Z(\omega) \sim R_{gap}$
 - Confirmed reduction of 5-6% of the transfer impedance because of ohmic losses in the ferrite $Z_t(\omega) = 2.68 \Omega$ instead of 2.83Ω .
 - estimate of the ohmic resistance of the ferrite $\sim 50.50 \Omega$

NB: the expected value 2.83Ω of the spare WCM gap impedance results from the parallel of 3.0 and 50Ω .



$$Z(\omega) = \frac{V_{out}(\omega)}{I_{beam}(\omega)} [\Omega]$$



SwissFEL WCM transfer impedance $Z_t(\omega)$?

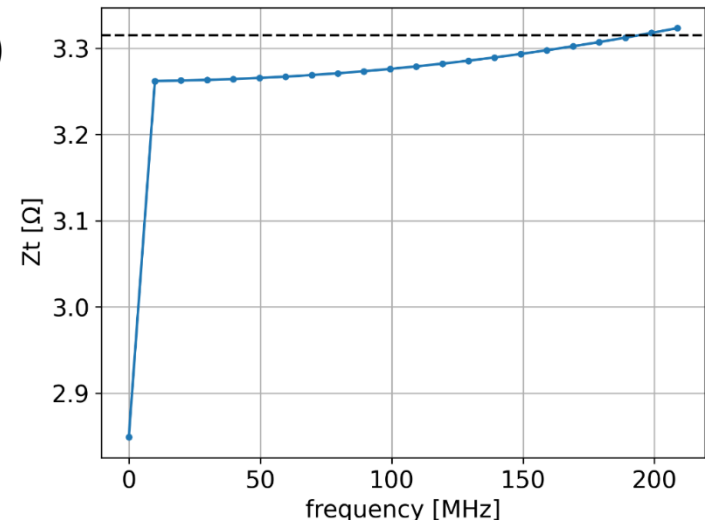
Direct measurement of transfer function of the SwissFEL WCM not possible.

Possible Solution:

- Replace the WCM currently installed at SwissFEL with the prototype WCM which is now fully characterized.
- Get Z_t from a CST simulation under hypothesis of two resistors disconnected and dispersive ferrite (Simulation parameters: $R_{\text{gap}} = 3.31 \Omega$, 25 ps bunch length, $Q = 200$ pC)

➤ to compensate ohmic losses in ferrite instead of $R_{\text{gap}} = 1/(1/3.55 + 1/50) = 3.31 \Omega$, the best up to date estimate of the transfer impedance are:

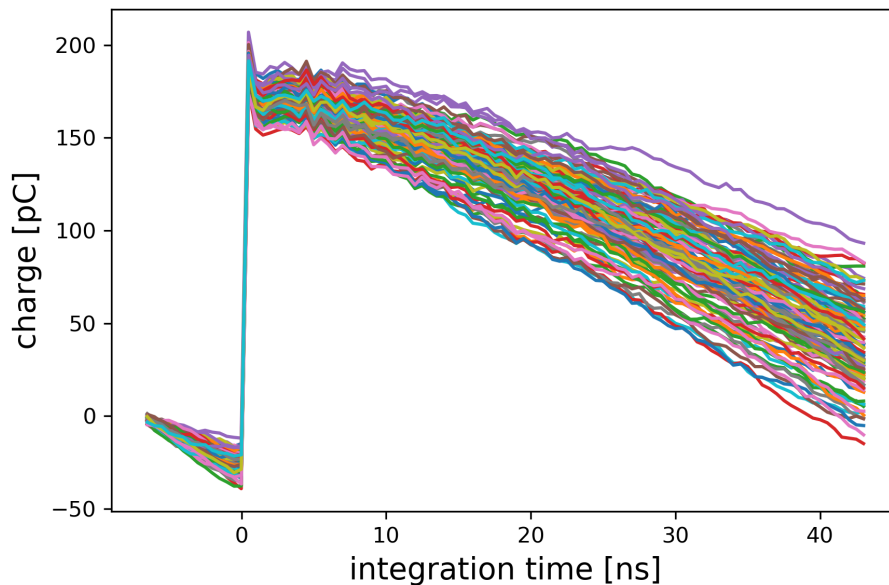
- $R_t \approx 3.26 \Omega$ CST prediction (near-DC value of the curve)
- $R_t \approx 3.11 \Omega$ (spare WCM VNA measurements)
- CST prediction sensitive to the permeability model of the ferrite
- To date, optimistic estimate of the incertitude on the WCM calibration parameter (R_t) about +/-5%



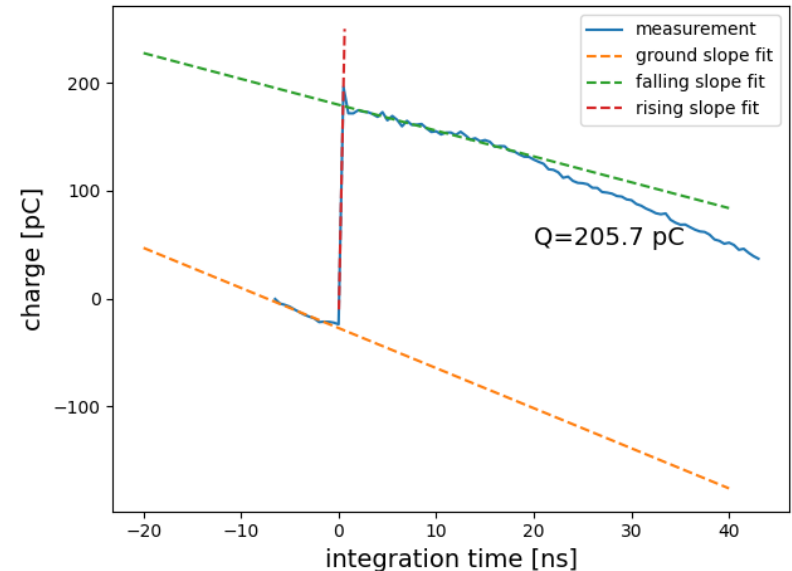
SwissFEL WCM: waveform signal integration and charge results

200 pC (charge readout of first turbo ICT)

$R_t = 3.26 \Omega$ (derived from SwissFEL WCM Zt simulation, considering dispersive ferrite)



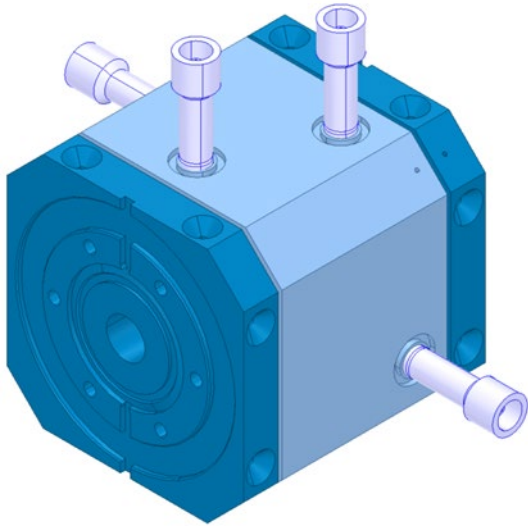
We integrate a background signal. Slopes are approximately linear.



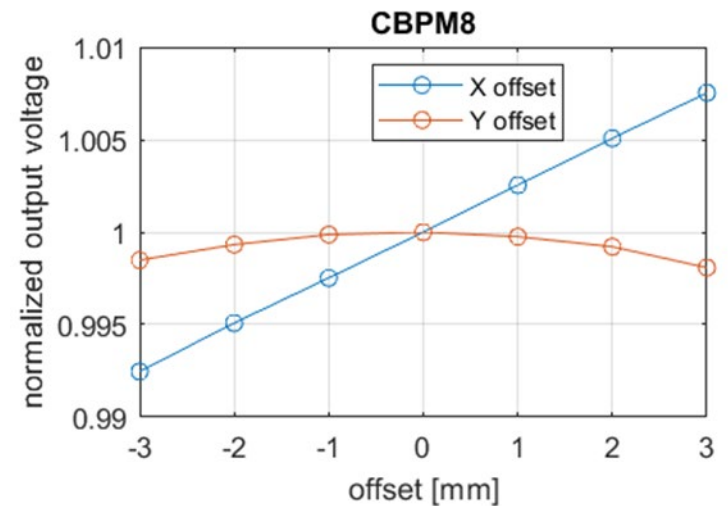
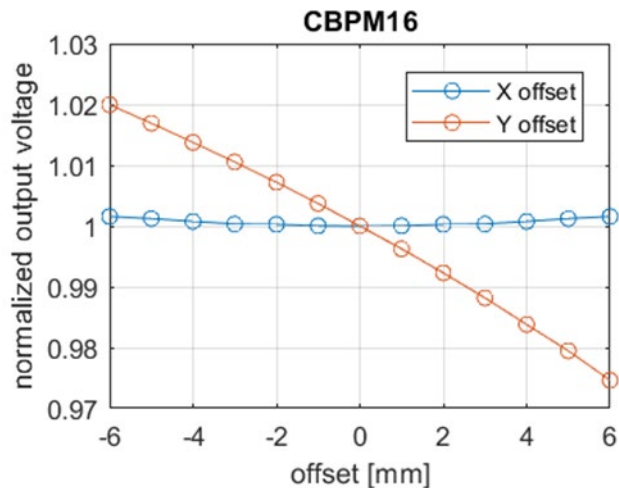
Still possible to measure the charge with our method using a linear fit!

Adapted idea: We extrapolate the charge and background signal contribution back to the time where the bunch was incident.

Cavity Beam position Monitor (CBPM)



- Two cavity device
- Reference cavity is designed to get an output signal proportional to the beam charge (monopole mode).
- Dependence on beam position is negligible (TM010 mode).
- We used:
 - CBPM16 type (low-Q).
 - CBPM8 type (high-Q)



Cavity BPM and charge measurement

BPM output signal measured with a 16GHz, 40Gs/s oscilloscope.

Bandpass filter at the BPM output to isolate the cavity fundamental mode (TM010) signal.

BPM type	TM010 frequency	Low-pass filter cutoff frequency
CBPM16	3.284 GHz	4.8 GHz
CBPM8	4.926 GHz	6.0 GHz

Voltage induced in the TM010 cavity mode and available at the cavity output port is:

$$V_{out}(t) = q\omega \sqrt{\frac{Z}{Q_e} R/Q} e^{-\frac{\omega t}{2Q_L}} \cos(\omega t)$$

(e.g. see : **Cavity Beam Position Monitors**, R. Lorenz)

q(charge); Z(50Ω, impedance cavity output line); ω (frequency of cavity mode TM010); R/Q (parameter depending on cavity geometry); Q_e (external quality factor); Q_L (loaded quality factor)

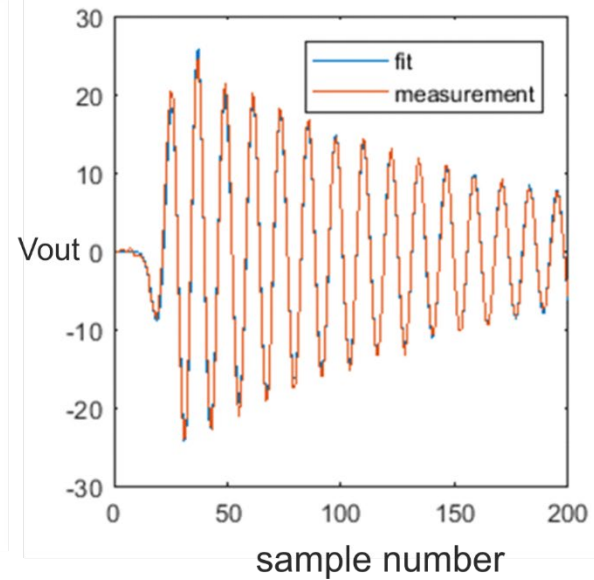
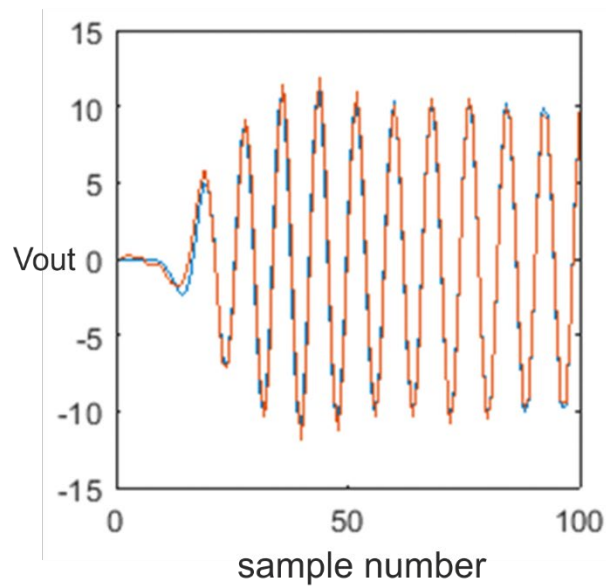
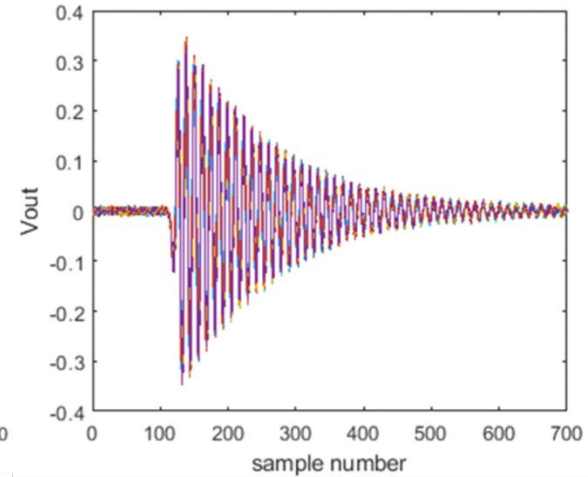
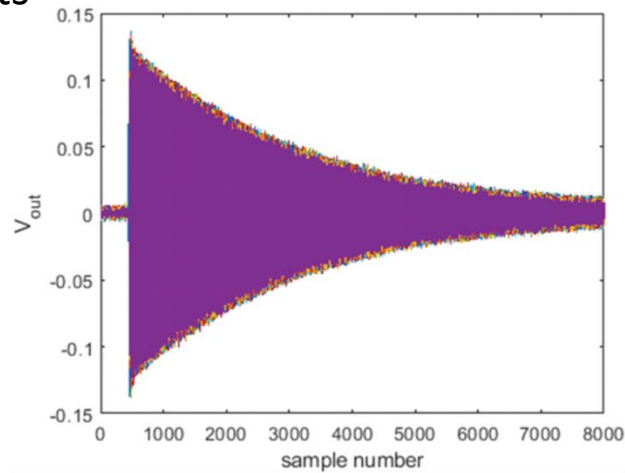
For every single BPM ω, Q_e and Q_L have been measured with VNA.

R/Q is estimated with reliable numerical codes (HFSS and CST, same result).

To better reproduce the measured signal, the expression above is also convolved with a low-pass filter function, same cutoff frequency as the filter used for measurements.

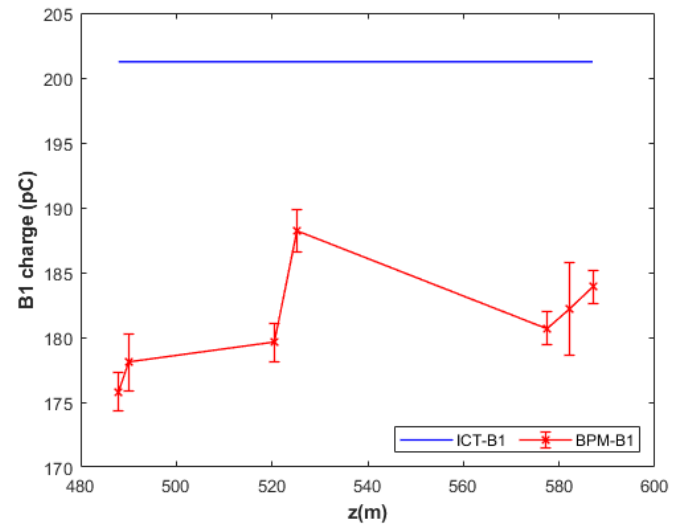
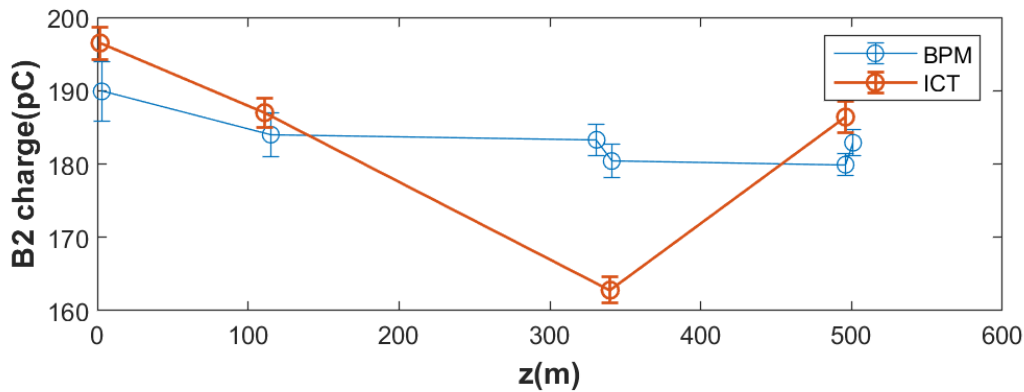
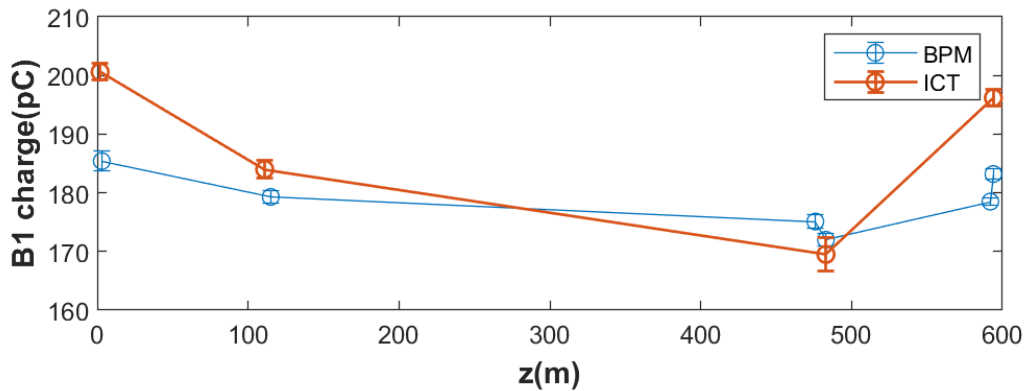
Cavity BPM charge measurements

- high Q (left) and low Q (right) BPM: waveforms measured with the oscilloscope and fit results





Beam charge measurements at SwissFEL



With respect to first ICT (~200 pC) about 20pC smaller mean charge readout from cavity BPMs:

Left (B1) → (10+/-3)%

Right (B1) → (10+/-2)%

Left: Charge measurements (B1, B2) of cavity BPMs and closest ICT in ARAMIS and ATHOS (measurements not simultaneous)

Right: charge measurements (B1) of cavity BPMs in high energy part of ARAMIS compared with average value of charge readout from the first Turbo-ICT-2 at the gun



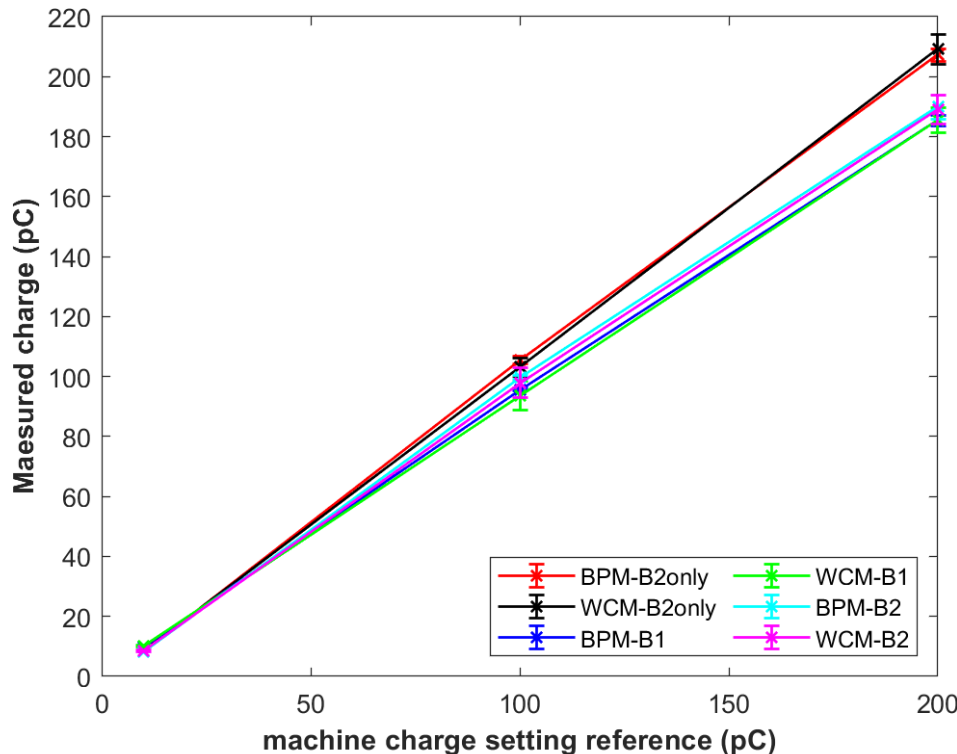
Beam charge measurements at SwissFEL

Simultaneous charge readouts of first cavity BPM and at the gun and the WCM for variable charge and three different gun settings: (1) Only bunch1; measured bunch 1 in presence of bunch-2; measured bunch-2 in presence of bunch-1.

Nominal charge	200pC	100 pC	10 pC
WCM/BPM bunch-2 only	1.0092	0.9773	1.0361
WCM/BPM bunch-1	1.0011	0.9770	1.0204
WCM/BPM bunch-2	0.9953	0.9819	1.0341

WCM transfer impedance

estimate $R_t \approx 3.26 \Omega$ (CST prediction)



In the case bunch-1 at 200 pC, the relative percentage difference of the charge readout of the 1st cavity BPM w.r.t. the 1st ICT is about:

(8+/-1)%

➤ WCM:

- experimental characterization (VNA) and numerical modelling (CST, HFSS) but still uncertainty on the calibration (+/-5%, very optimistic).
- Further characterization needed to solve the uncertainty
- Main problem: no VNA transfer function measurements possible in the SwissFEL WCM

➤ Cavity BPM:

- New method developed and implemented at SwissFEL for absolute charge measurements
- Robust and statistically consistent reliability for charge measurements at SwissFEL
- The aggregate results of the campaign of measurements with cavity BPM give us a calibration reference for alignment of all the charge monitors in SwissFEL
- **Calibration procedure of charge monitors for bunch-1: apply a correction factor (9+/-2)% to the charge readout measured by the first Turbo-ICT-2 at the gun and align all the other charge monitors under a condition of full transmission along the entire machine**