

AN ANALOG RF GAP VOLTAGE REGULATION SYSTEM FOR THE ADVANCED PHOTON SOURCE STORAGE RING*

D. Horan[#] and E. Cherbak

Argonne National Laboratory, 9700 South Cass Avenue, Argonne, IL 60439 U.S.A.

Abstract

An analog rf gap voltage regulation system has been designed and built at Argonne National Laboratory to maintain constant total storage ring rf gap voltage, independent of beam loading and cavity tuning effects. The design uses feedback control of the klystron mod-anode voltage to vary the amount of rf power fed to the storage ring cavities. The system consists of two independent feedback loops, each regulating the combined rf gap voltages of eight storage ring cavities by varying the output power of either one or two rf stations, depending on the mode of operation. It provides full operator control and permissive logic to permit feedback control of the rf system output power only if proper conditions are met. The feedback system uses envelope-detected cavity field probe outputs as the feedback signal. Two different methods of combining the individual field probe signals were used to generate a relative DC level representing one-half of the total storage ring rf voltage, an envelope-detected vector sum of the field probe rf signals, and the DC sum of individual field probe envelope detector outputs. The merits of both methods are discussed. The klystron high-voltage power supply (HVPS) units are fitted with an analog interface for external control of the mod-anode voltage level, using a four-quadrant analog multiplier to modulate the HVPS mod-anode voltage regulator set-point in response to feedback system commands.

1 APS GAP VOLTAGE CONTROL REQUIREMENTS

The APS utilizes a 7-GeV storage ring to generate synchrotron light for material research. The ring is designed to store 300 mA and has been operated routinely at 102 mA maximum current to date. The storage ring uses 16 single-cell cavities, arranged in groups of four at discrete sectors, to generate 9.4 megavolts of total rf gap voltage. Four 1-MW rf stations are used to supply power to the cavities, and a waveguide switching/combining system allows operation of the storage ring with any two or more of the four rf stations simultaneously.

Because the maximum beam loading in the storage ring cavities will represent a coupling coefficient of approximately 4, the amount of rf power required to maintain 9.4 megavolts of total rf gap voltage varies widely depending on the amount of stored current [1].

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[#] Email: horan@aps.anl.gov

The present method used to regulate total storage ring gap voltage is a “control law” software program, utilizing two separate software amplitude control loops. This system has worked well, but it can only sample the cavity field probe powers and make adjustments to the rf system output power at a rate no faster than 1 Hz. This slow data acquisition and transmission rate has caused delays in reducing the output power of the rf stations, resulting in rf system trips. The trips occur when the storage ring beam is suddenly dumped or lost, resulting in an instantaneous increase in the rf power dissipation of the rf cavities by an amount equal to the beam loading effect. This sudden increase in power can degrade cavity vacuum and cause damage to cavity components such as tuners and couplers. The analog automatic gain control (AGC) system was developed to provide fast and accurate control of the rf system power output as a function of stored beam current intensity.

2 ANALOG REGULATION SYSTEM OVERVIEW

The analog gap voltage regulation system is a true DC-coupled feedback system for maintaining constant rf gap voltage amplitude in the APS storage ring cavities (see Fig. 1). The system consists of two identical and independent amplitude-control feedback loops. Each loop regulates the combined gap voltage of eight storage ring cavities (a sector-pair) by making real-time adjustments of the rf power into the cavities in response to cavity beam-loading effects. This maintains agreement between the combined envelope-detected field-probe powers and an operator-selected gap-voltage setpoint.

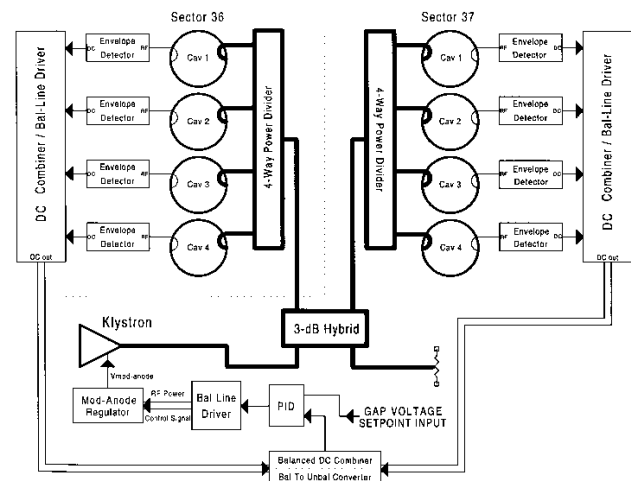


Figure 1: Analog rf gap voltage regulation system

At every sector, each of the four cavity field probes drives a dedicated envelope detector, the DC output of which is then converted from single-ended to balanced output by an active line converter. The balanced outputs of all four balanced converters are then combined at each sector using a passive resistor network. This DC sum is sent to another DC-combiner chassis that sums the two sector-pair DC outputs together and generates a DC signal directly proportional to the combined field probe power in eight cavities. This signal is converted to single-ended topology and applied to the input of a VXI-based PID controller, which allows for remote control of proportional, integral, and differential (PID) gain in the feedback loop, plus remote loop setpoint adjustment. The PID controller output is then converted from single-ended to a pair of equal-amplitude balanced outputs, which are then each sent via single-pair cable to the external mod-anode voltage control input of the two rf stations that can drive the sector-pair of cavities. This signal controls the rf system output power by increasing or decreasing the operator-selected klystron mod-anode voltage regulator setpoint value.

The AGC feedback system also includes control logic that permits feedback control of the rf system output powers under conditional constraints. Each rf station has a logic control chassis that allows feedback to be engaged on the rf station only if all of the following conditions are met:

- system operator consciously selects gap voltage feedback operation,
- the collector-dissipation interlock is set [2],
- the particular rf system output is switched into the ring,
- a minimum of seven out of the eight cavities in the sector-pair are in tune, and
- the klystron has a sufficient level of rf drive.

If any of these conditions are not met, a situation is defined where feedback control of the rf system output power either is not desired or not possible. The control logic chassis will then disable the AGC feedback control within 6 ms. This reaction time has proven fast enough to prevent klystron outgassing caused by sudden large increases in beam current when the AGC loop is suddenly opened.

3 RF SYSTEM POWER OUTPUT CONTROL

The AGC feedback system uses a four-quadrant analog multiplier [3] on an interface card to externally control the klystron mod-anode voltage (see Fig. 2). The DC control signal from the AGC feedback system is used as a value by which to multiply the operator-selected mod-anode regulator setpoint voltage, thus providing the ability to increase and decrease the klystron beam current in response to the feedback system commands. The external mod-anode control card converts the balanced-

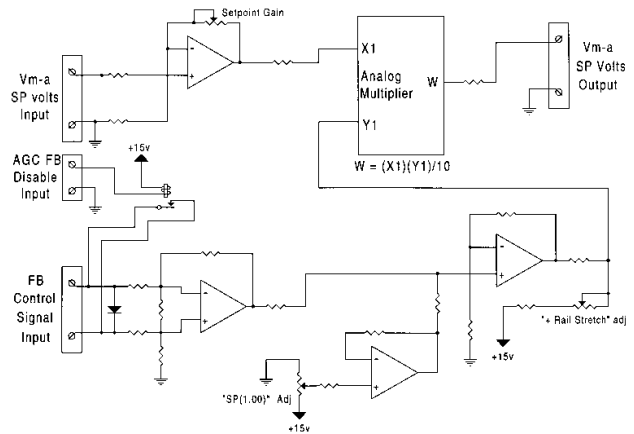


Figure 2: External mod-anode control interface

line feedback control signal to single-ended, and also diode-clips the feedback control signal in the negative direction so that the analog multiplier cannot generate a mod-anode setpoint voltage significantly lower than the operator-selected setpoint value. It provides DC offset controls to optimize the available range of the setpoint multiplication to a maximum of 1.5, which will result in approximately 4 dB of klystron rf output power control range. The use of an analog multiplier for this function has two discrete advantages, (1) the AGC feedback system can never increase the klystron mod-anode voltage by more than approx. 1.5, and (2) the operator still has control of the baseline value for mod-anode setpoint. The feedback is disabled on the external control card by a fast reed relay that shorts the analog feedback control signal input when the feedback logic control chassis detects an operating condition that is not compatible with engaged feedback. The Experimental Physics Industrial Control System (EPICS) [4] remote-control screens have been developed to allow for remote operator control and monitoring of the feedback control logic chassis and system DC operating points from all operating locations.

4 FEEDBACK SYSTEM PERFORMANCE

Two methods of generating the analog feedback system input signal were tested to determine which would perform best for this application. One method used the vector-sum of eight field probe rf signals (see Fig. 3), which was then envelope-detected to develop a DC voltage proportional to the amplitude of the combined field probe rf signals. The other method used the DC-sum of eight individual field-probe envelope detector outputs (see Fig. 1). The performance of both analog feedback system methods was measured. During these tests, eight storage ring cavities were under analog-feedback gap voltage control, while the other eight cavities were regulated using the traditional software control law gap-voltage regulation system.

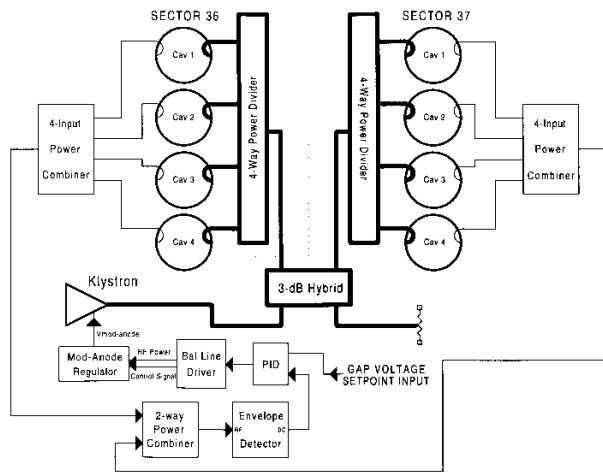


Figure 3: Rf vector-sum feedback input signal generation

It was found that using the vector-sum of eight field-probe rf signals as the feedback system input resulted in very poor gap voltage regulation in response to beam loading. At a stored current of 100 mA, the combined gap voltage of the eight cavities under analog control had sagged approximately 14% from injection-power levels.

This poor regulation was caused by phase-to-amplitude cross-modulation of the field probe rf signals when they were combined in the rf regime. Because each of the storage ring cavities and their associated tuner control systems react differently to cavity beam loading effects, a vector-sum of individual cavity field probe signals will always contain an amplitude distortion generated by the differential phase shifts of the individual signals. This amplitude distortion affects the gap voltage regulation by allowing the beam to unevenly load the cavities without causing a corresponding reduction in the vector-sum field-probe signal applied to the gap voltage feedback system input. Phase-to-amplitude cross-modulation of the combined field-probe signals creates an artificial increase in total field probe signal level; therefore the feedback system does not call for more rf power to combat the beam loading effects, and the gap voltage sags as more beam is stored.

Using the DC-sum of individual field-probe envelope detector outputs as the feedback system input produced much better gap voltage regulation. By combining DC signals proportional to the amplitude of the individual cavity field probe powers, differential phase errors between the cavity field probe rf signals are ignored; the resulting signal is a very sensitive indicator of the combined cavity Q reduction caused by beam loading. It allowed the feedback system to accurately detect beam loading and increase the rf power to the cavities in order to maintain 9.4-MV total gap voltage, with no detectable sag from injection to 102 mA stored current.

Closed-loop frequency response measurements on the AGC feedback system were performed (see Fig. 4). The

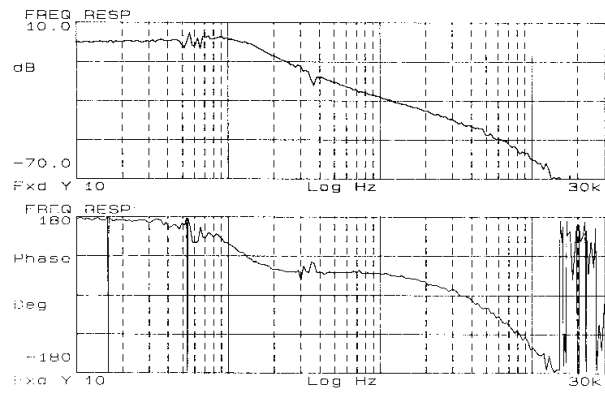


Figure 4: AGC system closed-loop response test

rapid roll-off of the loop frequency response above approximately 150 Hz is caused by the limited operating bandwidth of the mod-anode regulator.

5 CONCLUSION

The analog gap voltage regulation system has been successful in providing good storage ring gap voltage regulation in response to beam loading effects up to 102 mA stored beam. This system will reduce the number of klystron and cavity-related vacuum trips due to overpower events when beam is lost or dumped. Closed-loop frequency response tests indicate that the loop operates in a stable region and has adequate bandwidth for the application. This system will be fully installed at APS by April of 1999.

6 ACKNOWLEDGMENTS

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7 REFERENCES

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